P11.35
(a) $L_{i}=m v \mathrm{l} \quad \sum \tau_{\mathrm{ext}}=0$, so $L_{f}=L_{i}=m v$
$L_{f}=(m+M) v_{f} l$
$v_{f}=\left(\frac{m}{m+M}\right) v$
(b) $\quad K_{i}=\frac{1}{2} m v^{2}$
$K_{f}=\frac{1}{2}(M+m) v_{f}^{2}$
$v_{f}=\left(\frac{m}{M+m}\right) v \Rightarrow$ velocity of the bullet and block


FIG. P11.35

Fraction of $K$ lost $=\frac{\frac{1}{2} m v^{2}-\frac{1}{2} \frac{m^{2}}{M+m} v^{2}}{\frac{1}{2} m v^{2}}=\frac{M}{M+m}$
P11.36 For one of the crew,

$$
\begin{gathered}
\sum F_{r}=m a_{r}: n=\frac{m v^{2}}{r}=m \omega_{i}^{2} r \\
\text { We require } n=m g \text {, so } \omega_{i}=\sqrt{\frac{g}{r}} \\
\text { Now, } \quad I_{i} \omega_{i}=I_{f} \omega_{f} \\
{\left[5.00 \times 10^{8} \mathrm{~kg} \cdot \mathrm{~m}^{2}+150 \times 65.0 \mathrm{~kg} \times(100 \mathrm{~m})^{2}\right] \sqrt{\frac{g}{r}}=\left[5.00 \times 10^{8} \mathrm{~kg} \cdot \mathrm{~m}^{2}+50 \times 65.0 \mathrm{~kg}(100 \mathrm{~m})^{2}\right] \omega_{f}} \\
\left(\frac{5.98 \times 10^{8}}{5.32 \times 10^{8}}\right) \sqrt{\frac{g}{r}}=\omega_{f}=1.12 \sqrt{\frac{g}{r}} \sqrt{r} \\
\text { Now, } \quad\left|a_{r}\right|=\omega_{f}^{2} r=1.26 g=12.3 \mathrm{~m} / \mathrm{s}^{2}
\end{gathered}
$$

P11.46
(a) The radial coordinate of the sliding mass is $r(t)=(0.0125 \mathrm{~m} / \mathrm{s}) t$. Its angular momentum is

$$
\begin{aligned}
L & =m r^{2} \omega=(1.20 \mathrm{~kg})(2.50 \mathrm{rev} / \mathrm{s})(2 \pi \mathrm{rad} / \mathrm{rev})(0.0125 \mathrm{~m} / \mathrm{s})^{2} t^{2} \\
\text { or } \quad L & =\left(2.95 \times 10^{-3} \mathrm{~kg} \cdot \mathrm{~m}^{2} / \mathrm{s}^{3}\right) t^{2}
\end{aligned}
$$

The drive motor must supply torque equal to the rate of change of this angular momentum:

$$
\tau=\frac{d L}{d t}=\left(2.95 \times 10^{-3} \mathrm{~kg} \cdot \mathrm{~m}^{2} / \mathrm{s}^{3}\right)(2 t)=(0.00589 \mathrm{~W}) t
$$

(b) $\quad \boldsymbol{\tau}_{f}=(0.00589 \mathrm{~W})(440 \mathrm{~s})=2.59 \mathrm{~N} \cdot \mathrm{~m}$
(c) $\quad \mathrm{P}=\tau \omega=(0.00589 \mathrm{~W}) t(5 \pi \mathrm{rad} / \mathrm{s})=(0.0925 \mathrm{~W} / \mathrm{s}) t$
(d) $\quad \mathrm{P}_{f}=(0.0925 \mathrm{~W} / \mathrm{s})(440 \mathrm{~s})=40.7 \mathrm{~W}$
(e) $\quad T=m \frac{v^{2}}{r}=m r \omega^{2}=(1.20 \mathrm{~kg})(0.0125 \mathrm{~m} / \mathrm{s}) t(5 \pi \mathrm{rad} / \mathrm{s})^{2}=(3.70 \mathrm{~N} / \mathrm{s}) t$
(f) $\quad W=\int_{0}^{440 \mathrm{~s}} \mathrm{P} d t=\int_{0}^{440 \mathrm{~s}}(0.0925 \mathrm{~W} / \mathrm{s}) t d t=\frac{1}{2}\left(0.0925 \mathrm{~J} / \mathrm{s}^{2}\right)(440 \mathrm{~s})^{2}=8.96 \mathrm{~kJ}$
(g) The power the brake injects into the sliding block through the string is

$$
\begin{aligned}
\mathbf{P}_{b} & =\mathbf{F} \cdot \mathbf{v}=T v \cos 180^{\circ}=-(3.70 \mathrm{~N} / \mathrm{s}) t(0.0125 \mathrm{~m} / \mathrm{s})=-(0.0463 \mathrm{~W} / \mathrm{s}) t=\frac{d W_{b}}{d t} \\
W_{b} & =\int_{0}^{440 \mathrm{~s}} \mathrm{P}_{b} d t=-\int_{0}^{440 \mathrm{~s}}(0.0463 \mathrm{~W} / \mathrm{s}) t d t \\
& =-\frac{1}{2}(0.0463 \mathrm{~W} / \mathrm{s})(440 \mathrm{~s})^{2}=-4.48 \mathrm{~kJ}
\end{aligned}
$$

(h) $\quad \sum W=W+W_{b}=8.96 \mathrm{~kJ}-4.48 \mathrm{~kJ}=4.48 \mathrm{~kJ}$

Just half of the work required to increase the angular momentum goes into rotational kinetic energy. The other half becomes internal energy in the brake.

P11.50 (a) Angular momentum is conserved:

$$
\begin{aligned}
& \frac{m v_{i} d}{2}=\left(\frac{1}{12} M d^{2}+m\left(\frac{d}{2}\right)^{2}\right) \omega \\
& \omega=\frac{6 m v_{i}}{M d+3 m d}
\end{aligned}
$$

(b) The original energy is $\frac{1}{2} m v_{i}^{2}$.


FIG. P11.50
The final energy is

## Continued on next page

$$
\frac{1}{2} I \omega^{2}=\frac{1}{2}\left(\frac{1}{12} M d^{2}+\frac{m d^{2}}{4}\right) \frac{36 m^{2} v_{i}^{2}}{(M d+3 m d)^{2}}=\frac{3 m^{2} v_{i}^{2} d}{2(M d+3 m d)} .
$$

The loss of energy is

$$
\frac{1}{2} m v_{i}^{2}-\frac{3 m^{2} v_{i}^{2} d}{2(M d+3 m d)}=\frac{m M v_{i}^{2} d}{2(M d+3 m d)}
$$

and the fractional loss of energy is

$$
\frac{m M v_{i}^{2} d 2}{2(M d+3 m d) m v_{i}^{2}}=\frac{M}{M+3 m} .
$$

P11.54 For the cube to tip over, the center of mass (CM) must rise so that it is over the axis of rotation AB . To do this, the CM must be raised a distance of $a(\sqrt{2}-1)$.

$$
\therefore M g a(\sqrt{2}-1)=\frac{1}{2} I_{\mathrm{cube}} \omega^{2}
$$



From conservation of angular momentum,

$$
\begin{aligned}
& \frac{4 a}{3} m v=\left(\frac{8 M a^{2}}{3}\right) \omega \\
& \omega=\frac{m v}{2 M a} \\
& \frac{1}{2}\left(\frac{8 M a^{2}}{3}\right) \frac{m^{2} v^{2}}{4 M^{2} a^{2}}=\operatorname{Mga}(\sqrt{2}-1) \\
& v=\frac{M}{m} \sqrt{3 g a(\sqrt{2}-1)}
\end{aligned}
$$



FIG. P11.54

Chapter Twelve: Static Equilibrium and Elasticity

## SOLUTIONS TO PROBLEMS

P12.1 To hold the bat in equilibrium, the player must exert both a force and a torque on the bat to make

$$
\sum F_{x}=\sum F_{y}=0 \text { and } \sum \tau=0
$$

$\sum F_{y}=0 \Rightarrow F-10.0 \mathrm{~N}=0$, or the player must exert a net upward force of $F=10.0 \mathrm{~N}$

To satisfy the second condition of equilibrium, the player must exert an applied torque $\tau_{a}$ to make $\sum \tau=\tau_{a}-(0.600 \mathrm{~m})(10.0 \mathrm{~N})=0$. Thus, the required torque is


FIG. P12.1

$$
\tau_{a}=+6.00 \mathrm{~N} \cdot \mathrm{~m} \text { or } 6.00 \mathrm{~N} \cdot \mathrm{~m} \text { counterclockwise }
$$

P12.6 Let $\sigma$ represent the mass-per-face area. A vertical strip at position $x$, with width $d x$ and height $\frac{(x-3.00)^{2}}{9}$ has mass

$$
d m=\frac{\sigma(x-3.00)^{2} d x}{9}
$$

The total mass is

$$
\begin{aligned}
& M=\int d m=\int_{x=0}^{3.00} \frac{\sigma(x-3)^{2} d x}{9} \\
& M=\left(\frac{\sigma}{9}\right)^{3.00}\left(x_{0}^{2}-6 x+9\right) d x \\
& M=\left(\frac{\sigma}{9}\right)\left[\frac{x^{3}}{3}-\frac{6 x^{2}}{2}+9 x\right]_{0}^{3.00}=\sigma
\end{aligned}
$$



FIG. P12.6

The $x$-coordinate of the center of gravity is

$$
x_{\mathrm{CG}}=\frac{\int x d m}{M}=\frac{1}{9 \sigma} \int_{0}^{3.00} \sigma x(x-3)^{2} d x=\frac{\sigma}{9 \sigma} \int_{0}^{3.00}\left(x^{3}-6 x^{2}+9 x\right) d x=\frac{1}{9}\left[\frac{x^{4}}{4}-\frac{6 x^{3}}{3}+\frac{9 x^{2}}{2}\right]_{0}^{3.00}=\frac{6.75 \mathrm{~m}}{9.00}=0.750 \mathrm{~m}
$$

P12.19 (a) $T_{e} \sin 42.0^{\circ}=20.0 \mathrm{~N} \quad T_{e}=29.9 \mathrm{~N}$
(b) $T_{e} \cos 42.0^{\circ}=T_{m} T_{m}=22.2 \mathrm{~N}$

P12.25 To find $U$, measure distances and forces from point A. Then, balancing torques,

$$
(0.750) U=29.4(2.25) \quad U=88.2 \mathrm{~N}
$$

To find $D$, measure distances and forces from point $B$. Then, balancing torques,

$$
(0.750) D=(1.50)(29.4) \quad D=58.8 \mathrm{~N}
$$

Also, notice that $U=D+F_{g}$, so $\sum F_{y}=0$.

P12.42 Call the normal forces $A$ and $B$. They make angles $\alpha$ and $\beta$ with the vertical.

$$
\begin{array}{ll}
\sum F_{x}=0: & A \sin \alpha-B \sin \beta=0 \\
\sum F_{y}=0: & A \cos \alpha-M g+B \cos \beta=0
\end{array}
$$

Substitute $B=\frac{A \sin \alpha}{\sin \beta}$


$$
\begin{aligned}
& A \cos \alpha+A \cos \beta \frac{\sin \alpha}{\sin \beta}=M g \\
& A(\cos \alpha \sin \beta+\sin \alpha \cos \beta)=M g \sin \beta \\
& A=M g \frac{\sin \beta}{\sin (\alpha+\beta)} \\
& B=M g \frac{\sin \alpha}{\sin (\alpha+\beta)}
\end{aligned}
$$



FIG. P12.42
P12.46 $\sum \tau_{\text {point } 0}=0$ gives

$$
\begin{array}{r}
\left(T \cos 25.0^{\circ}\right)\left(\frac{31}{4} \sin 65.0^{\circ}\right)+\left(T \sin 25.0^{\circ}\right)\left(\frac{31}{4} \cos 65.0^{\circ}\right) \\
=(2000 \mathrm{~N})\left(I \cos 65.0^{\circ}\right)+(1200 \mathrm{~N})\left(\frac{1}{2} \cos 65.0^{\circ}\right)
\end{array}
$$

From which, $T=1465 \mathrm{~N}=1.46 \mathrm{kN}$
From $\sum F_{x}=0$,

$$
H=T \cos 25.0^{\circ}=1328 \mathrm{~N}(\text { toward right })=1.33 \mathrm{kN}
$$



FIG. P12.46
From $\sum F_{y}=0$,

$$
V=3200 \mathrm{~N}-T \sin 25.0^{\circ}=2581 \mathrm{~N}(\text { upward })=2.58 \mathrm{kN}
$$

